WRIST JOINT MOTIONS AND REACTION FORCES IN WHEELCHAIR USERS WITH PARAPLEGIA AND TETRAPLEGIA DURING OVERGROUND PROPULSION
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ABSTRACT

Twenty-six wheelchair users with spinal cord injuries participated in this cross-sectional, repeated-measures study. The objective was to investigate differences in wrist joint forces and motions between users with paraplegia and tetraplegia during overground propulsion. A secondary objective was to evaluate group differences over surfaces and speeds experienced in the built environment. Participants with tetraplegia propelled with higher peak forces and flexion/extension ranges of motion (ROM). Differences were greatest during conditions that induced higher rolling resistances – carpet at unnatural propulsion speeds. These biomechanical differences are likely adaptations needed to overcome hand and wrist paralysis and could lead to secondary injury. Interventions such as orthotics or wheelchair modifications that optimize wrist biomechanics may reduce the risk of upper-extremity injury in individuals with tetraplegia; further development and testing of such interventions is warranted.

INTRODUCTION

Wrist and hand repetitive strain injuries occur after chronic exposure to repetitive, forceful hand motions in awkward wrist postures (Barr, Barbe, & Clark, 2004). Wheelchair users with spinal cord injury (SCI) often place high loads on their wrists to perform activities of daily living such as propulsion; this activity also involves large and often extreme movements of the wrist (Boninger, Cooper, Robertson, & Rudy, 1997). Thus, it is no surprise that a high prevalence of wrist and hand pain exist in this population (Pentland & Twomey, 1994).

Wheelchair users with SCI adapt to their level of injury by altering propulsion biomechanics (Newsam, et al. 1999). Previous studies, however, have reported conflicting results with respect to wrist biomechanics between those with tetra- and paraplegia. (Newsam, et al. 1999; Finley, et al. 2004). These studies used different wheelchair ergometer setups to simulate propulsion; the frictional and inertial properties of each may have caused these discrepancies. Using an overground setup may better mimic the built environment and provide information that is more clinically-relevant (Cowan, Boninger, Sawatzky, Mazoyer, & Cooper, 2008).

The purpose of the present study was to investigate differences in wrist joint kinematics and kinetics between wheelchair users with paraplegia and tetraplegia during overground propulsion. A secondary purpose was to investigate how biomechanics varied when propelling over different surfaces at various speeds. It was hypothesized that wrist propulsive joint motions and forces would be greater in those with tetraplegia. Differences were hypothesized to be greatest during conditions with unnatural propulsion speeds and surfaces with high rolling-resistance (RR).

METHODS

Subject Recruitment

Participants were recruited through research registries, flyers, and word of mouth. They were included if they were between 18 and 65 years of age; had an SCI with residual paralysis for over one year; used a manual wheelchair as their primary means of mobility; were injured after age 15; and were primarily English speaking. Exclusion criteria included history of upper-extremity fractures or dislocations that had not fully recovered; upper-limb dysthetic pain from a syrinx or regional pain syndrome; not having a “quick-
Kinematic Data Collection

Participants propelled down a 15-meter runway over tile and medium-pile carpet at self-selected and targeted (1.5 meters/second) speeds. Five trials were performed per condition. A 20-camera VICON system captured the runway volume. Prior to propelling, participants were equipped with reflective markers on the acromion, trunk, medial and lateral epicondyles, ulnar and radial styloids, and 3rd metacarpal-phalangeal joint (Boninger, Cooper, Robertson, & Rudy, 1997); 8 additional markers in diamond-shaped patterns were added to the upper- and lower-arm. A SmartWheel, which detects handrim three-dimensional forces and moments (Cooper, Robertson, VanSickle, Boninger, & Shimada, 1997), was attached opposite a dummy wheel with identical handrim and treads.

Kinematic data were collected via VICON at 60 Hz and filtered using a 4th order zero-phase low-pass Butterworth filter with 7 Hz cutoff. Kinetic data were collected via the SmartWheel at 240 Hz and filtered using an 8th order zero-phase low-pass Butterworth filter with a 20 Hz cutoff frequency, then down-sampled to 60 Hz to match kinematics. Trials were split into start-up (first 3 strokes) and steady-state (all strokes after start-up).

A previously-described inverse dynamics model was created to transform handrim forces and moments to the wrist joint (Cooper, Boninger, Shimada, & Lawrence, 1999; Mercer et al., 2006). Handrim forces and moments were collected using a SmartWheel, then input into the model to calculate wrist joint reaction forces with respect to the global coordinate system. Kinetics were transformed to the wrist local coordinate system – the forearm. Joint coordinate systems and motions were defined as recommended by the International Society of Biomechanics (Figure 2; Wu, et al. 2005). Peak three-dimensional forces and moments were analyzed. Wrist compressive, ulnar/radial shear, and palm/dorsum shear forces were calculated from this model (Figure 2). Not all subjects ulnarily deviated or supinated their wrists, so radial deviation and pronation minimum and maximums were reported. Data from all steady-state strokes per trial were analyzed and averaged, and then all trials per condition were averaged.

Statistical Analysis

Significance was set a priori to α=.05. Normality was assessed using the Shapiro-Wilk test. Participants were dichotomized into those with paraplegia (T1 or below) or tetraplegia (C7 or above). Group demographic differences were tested using Fisher’s exact test (categorical) and independent t-tests (continuous). Between-subjects biomechanical differences were tested using two-way mixed analysis of variance. Independent variables included injury-level (between-subjects) and speed/surface condition (within-subjects). Dependent kinematic variables were peak wrist flexion, extension, maximum and minimum pronation and radial deviation, and ROM in each axis (Figure 2). Dependent kinetic variables included peak wrist resultant, compressive, palm to dorsum, and radial shear forces. To maximize statistical power with the small sample size it was decided not to apply corrections to these a priori tests. Following significant omnibus F-tests, univariate between-subjects ANOVAs were performed for each condition. Differences in velocity were also tested using two-way mixed ANOVA. Bonferroni corrections were applied to all post hoc tests.

Wrist forces correlated with body-weight (p<.05) and thus were weight-normalized. Velocities were different between surface/speed conditions (p<.05; Table 2). Wrist kinematics can change with variations in speed (Boninger et al., 1997), so joint motions were normalized to velocity.

Table 2. Average propulsion velocities for participants with paraplegia and tetraplegia, presented as means and standard deviations for cement and carpet surfaces at self-selected and targeted speeds.

<table>
<thead>
<tr>
<th>Surface-Speed</th>
<th>PP (N=18) M</th>
<th>PP (N=18) SD</th>
<th>TP (N=8) M</th>
<th>TP (N=8) SD</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cement-SS</td>
<td>1.63</td>
<td>0.28</td>
<td>1.70</td>
<td>0.30</td>
</tr>
<tr>
<td>Cement-targeted</td>
<td>1.66</td>
<td>0.14</td>
<td>1.67</td>
<td>0.38</td>
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<tr>
<td>Carpet-SS</td>
<td>1.47</td>
<td>0.23</td>
<td>1.55</td>
<td>0.38</td>
</tr>
<tr>
<td>Carpet-targeted</td>
<td>1.61</td>
<td>0.95</td>
<td>1.58</td>
<td>0.11</td>
</tr>
</tbody>
</table>

Notes. PP: Paraplegia. TP: Tetraplegia. SS: Self-selected. A main effect of condition was found, F(1.771,42.508)=4.195, p=.026, partial η²=.149. Post hoc differences were observed between cement and carpet at self-selected (p=.039) and targeted speeds (p=.027).
paralysis may have required this group to compensate by applying more force and increasing friction between palm and handrim. Additionally, flexor and extensor motor imbalances may have contributed to the higher ROMs in this study’s tetraplegia group.

**RESULTS**

**Participants**

Thirty-one manual wheelchair users were recruited. Three did not meet inclusion criteria and two had wrist data that could not be analyzed (both with paraplegia), leaving a sample size of 26. No demographic differences were found between groups (Tables 1). Injury levels of the participants with tetraplegia were C5 (N=2), C5/6 (N=1), and C7 (N=5).

**Between-Subjects Effects**

Omnibus F-tests indicated a main effect of injury-level on normalized flexion/extension ROM, FR, and palm to dorsum shear force (p<.05; Table 3). Post hoc univariate between-subjects F-tests indicated differences in peak ROM and FR (p=.0125; Table 3) on carpeted surfaces at targeted speed. Differences in palm to dorsum forces were significant on both cement and carpet at targeted speed (p<.0125; Table 3). Velocity differed between conditions (p<.05; Table 2), but not between injury-level groups.

**DISCUSSION**

Differences based on injury level were observed in wrist joint reaction forces and kinematics during propulsion over cement and carpeted surfaces. Participants with tetraplegia experienced greater wrist loading and ranges of motion. Reduced grip strength caused by upper-extremity paralysis may have required this group to compensate by applying more force and increasing friction between palm and carpeting that reduces RR and frictional and inertial differences may have potentially amplified these conditions. Although the fixed setup offers advantages, these interventions could take the form of orthotics or special wheelchair components, such as pushrim that work to increase friction and/or wrist stability.

Of importance are the biomechanical differences observed over carpet and at targeted speeds. Carpet increases RR at the targeted speed and may elicit an unnatural propulsion technique. Indeed, propulsion biomechanics have been observed to change with variations in RR (Cowan, Nash, Collinger, Koontz, & Boninger, 2006). Interventions that optimize hand and wrist biomechanics may improve function while decreasing risk of injury. These interventions could take the form of orthotics or special wheelchair components, such as pushrim that work to increase friction and/or wrist stability.

**Table 4. Propulsive wrist flexion/extension ranges of motion, resultant forces, and palm to dorsum shear forces during propulsion over cement and carpet at self-selected and targeted (1.5 m/s) speeds. Normalized data are presented as means and standard deviations with analysis of variance statistics. Raw values are in parentheses for reference.**

<table>
<thead>
<tr>
<th>Surface-Speed</th>
<th>Paraplegia (N=18)</th>
<th>Tetraplegia (N=8)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Palm to Dorsum Force</td>
<td></td>
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<td></td>
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<tr>
<td>Cement-SS</td>
<td>0.43 (30.1)</td>
<td>0.21 (13.7)</td>
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<tr>
<td>Cement-targeted</td>
<td>0.39 (28.8)</td>
<td>0.09 (9.7)</td>
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<tr>
<td>Carpet-SS</td>
<td>0.42 (32.2)</td>
<td>0.13 (13.2)</td>
</tr>
<tr>
<td>Carpet-targeted</td>
<td>0.48 (35.4)</td>
<td>0.12 (11.2)</td>
</tr>
<tr>
<td>Cement-SS</td>
<td>0.78 (57.1)</td>
<td>0.28 (21.0)</td>
</tr>
<tr>
<td>Cement-targeted</td>
<td>0.74 (55.3)</td>
<td>0.14 (15.7)</td>
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<tr>
<td>Carpet-SS</td>
<td>0.84 (63.4)</td>
<td>0.19 (22.5)</td>
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<tr>
<td>Carpet-targeted</td>
<td>0.86 (64.3)</td>
<td>0.18 (19.1)</td>
</tr>
<tr>
<td>Cement-SS</td>
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<td>0.28 (21.0)</td>
</tr>
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<tbody>
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<td>Carpet-targeted</td>
<td>0.86 (64.3)</td>
<td>0.18 (19.1)</td>
</tr>
</tbody>
</table>

Notes: SS: Self-selected. *Significant after Bonferroni correction (p<.0125). \( F(1,24)=10.727, p=.003, \) partial \( \eta^2=.309. \) \( F(1,24)=4.751, p=.039, \) partial \( \eta^2=.165. \) \( F(1,24)=6.552, p=.017, \) partial \( \eta^2=.214. \)
were higher than those from a previous study (Newsam et al. 1999). Finley et al. (2004) reported greater wrist forces than those in the current sample, and found significantly greater wrist joint forces in the group without upper limb impairment. It is possible the overground setup elicits a more natural technique that can compare to propulsion over surfaces found in the built environment. This may allow for results that are more clinically relevant and generalizable to the SCI population (Cowan et al., 2008).

**Limitations**

The sample size was disproportionate with respect to injury-level groups. This affected variability of the data and thus significance and generalizability of some of the tests. The laboratory setup, including VICON markers and the SmartWheel, may have altered natural propulsion style. Finally, the sample included highly independent wheelchair users who could complete a lengthy protocol. This is not characteristic of all wheelchair users with SCI and thus limits generalizability.

**CONCLUSIONS**

Differences existed in wrist kinematics between manual wheelchair users with tetraplegia and paraplegia. Participants with tetraplegia propelled with greater F/E ROM and wrist reaction forces. Differences were most prevalent in conditions that increased RR. Further testing is necessary to better understand how these differences impact the risk of injury. These finding also might help design interventions that could improve propulsion biomechanics in individuals with tetraplegia.

**ACKNOWLEDGEMENTS**

Funding was provided by VA Grant #B6252R. This material is based upon work supported by the National Science Foundation Graduate Research Fellowship (Grant #1247842). Any opinion, findings, and conclusions or recommendations expressed in this material are those of the authors and do not necessarily reflect the view of the National Science Foundation, Department of Veterans Affairs, or United States Government.

**REFERENCES**


